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ATKINS EPSRC

Finite Element Analysis of Soil Plug Behaviour within Open-Ended Piles

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Problem Statement

The main pile design methods for open-ended piles include the API RP2 GEO (2011), the UWA-05 and the ICP-05. Each consider the effects of the soil plug differently and this varies the length and cost of offshore foundations.

So how can we as an industry improve on this?



How is the soil plug currently understood to behave under the actions of axial load?



Which of these cases actually replicate the true behaviour of the soil plug?

To improve our understanding of this issue we turn to experimentation and the use of finite elements.

One of the main findings from these tests is that the plug is mobilised from the base upwards!

Application of the Model

Case study selected: 37m pile offshore Soil conditions: Cohesive

Design method:	API RP2 GEO (2011)
Pile stiffness:	Rigid
Plug stiffness:	Infinite
API capacity estimate: <u>19.61MN</u>	

enters the pile. around pile.

soil moves through pile.

LOAD

 $\frac{d\sigma_{pl}}{dz}A_{pl} + \tau_s P_e + \tau_{i,i}P_i + \tau_{e,i}P_e = 0$

-15000

-20000

Finite Element Model of an Open-Ended Pile

'A model can be created which links the following foundation components mathematically:

- the pile
- the plug
- the surrounding soil
- the end bearing on the pile
- the end bearing on the plug

 $A_p +$

Ultimate Compressive Capacity (kN)

6000 8000 10000 12000 14000 16000 18000 20000

- Total Capacity: API method

-Total Capacity: FEA (varied input)

- The internal interface
- The external interface

 $d\sigma_n$

dz



Forces in Pile Elements (kN)

-10000

-5000

0



Further work

- Compare results from program with database of case studies in sands and clays
- Update the existing end bearing capacity ulletrelationships for open-ended piles.
- Enhance model of plug considering partial drainage

